ZEIBRIGHT MINE EXTENSION PROJECT

PLACER and NEVADA COUNTIES, CALIFORNIA, USA

TP 17N, R 11E, BLOCKS 21, 27, 28

DATE: May, 2003

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SUMMARY

The Zeibright Mine is a former gold producer located in northeastern California along the border between Placer and Nevada counties in the Sierra Nevada mountain range (Figures 1, 8). The mine is within the Sierra Nevada gold-bearing area in the Emigrant Gap Mining District immediately east of the productive Grass Valley and Nevada City Gold Districts (Figure 4). The area is considered related to the Mother Lode structure, the northern limit of which is approximately 40 km (25 miles) to the south-southwest of the Ziebright Mine. Production from both placer, drift and lode gold mining operations in Placer and Nevada counties together comes to approximately 560 million dollars worth of gold from the 1850's through to the 1970's. The Zeibright Mine produced over 100,000 ounces gold from underground operations.

The Zeibright structure is a NNW-striking altered and mineralized dike or sill of granodioritic composition with an apparent strike length of over 5500m (18,000 feet). The structure contains gold-bearing quartz veining ranging in width from 0.3m (10 feet) to over 9m (30 feet). The structure, believed to be continuous, is exposed on either side of the mountain and has been mined by various owners, between 1867 and 1959, from the southern exposure operating as the Zeibright Mine.

Due to a tailings pond failure in the early 1940's, which destroyed a Pacific Gas and Electric's Drum Power Plant downstream on the Bear River, all milling in the Bear Valley was curtailed. The owners at the time continued development with the idea of tunnelling approximately 6000m further, to the north side of the mountain, where they could set up milling facilities in a former hydraulic mining pit - the Omega Mine. Tunnel development continued from the north (Omega Mine) and south adits (Zeibright Mine) until 1941 or 1942 when Newmont Mining Corporation shut down the mine completely. The adit had been tunnelled approximately 600m (1800') to the east from the Omega hydraulic pit to intersect the structure and a total of 2600m (8500') to the north from the existing Zeibright Mine workings. Approximately 2300m (7000') remains to link the two tunnels (Figure 3).

To this end, Stina Resources Limited has staked the ground covering the last 1300m (4000') of the Zeibright extension adit and the intervening ground to the Omega adit (Figure 2). This comprises a total of seven 8.4-hectare (20-acre) claims along the strike of the proposed tunnel continuation.

The mine's proximity to the Melones Fault zone (Figure 8) and it's location along strike form the Mother Lode system of mines as well as its similarity to the Spanish Mine property (Figure 1) to the north speak of Zeibright's potential.

The Zeibright property has a strong, mineralized structure with documented ore-grade mineralization. Assays from the last operator provide indications of ore in place with extensive development drifting. The north face of the adit, currently on the company's existing claims, was apparently left in ore. Sampling results, from Newmont Mining Corporation maps (Appendix I and II), indicate ore grade material (greater than 0.1 ounce per ton gold) in several locations along the adit that have not yet been developed. It is recommended that as the two existing adits are linked, drill stations be driven off the main adit to test ore shoots both above and below the adit level. Drilling will also confirm that the north and south adits are indeed on the same structure, or possibly on related en echelon structures, and will identify the existence of parallel structures. Underground drilling is preferable to surface drilling as up to 200m (>650 feet) of Tertiary volcanic ashflow caps the hostrock between the Zeibright and Omega adits. This approach will enable bulk sampling, as well as open opportunities for cost-effective exploration drilling from underground to define vertical extent of existing and newly-defined ore shoots. Probing for potential parallel structures can also be achieved with this tactic. At least initially, bulk samples should be custom milled for metallurgical testing. The company should be investigating possible contacts for custom milling.

Figure 1. Location Map of Zeibright Mine Property

Given the very strong possibility of parallel structures, it is recommended that the company consider staking a wider band of claims along either side of the dike extension.

INTRODUCTION AND TERMS OF REFERENCE

Stina Resources Limited has commissioned this report to highlight and summarize the history of the work done to date on this gold property as well as to provide direction for its future exploration plans. Limited rock exposure meant that the author relied heavily upon published reports, government maps, private reports (mostly from Newmont Mining Corporation and existing mine reports), geology maps and assay sections. The author spent one day on the property with Dennis LaPrairie, P.Eng., who has spent several years accumulating data and surface rights information. This report is required by the Toronto Stock Exchange to fulfill the Technical Report requirement (43-101) for acceptance as a property of merit.

Data used came from Newmont Mining Corporation maps and reports that were acquired by Dennis LaPrairie. Stope sections, assay maps, survey data and level plans were among the maps recovered. Government maps and reports were also used in conjunction with reports previously written on this property. The geology section written by R. Cuffney was invaluable as little information was found pertaining to the immediate area. Other sources of information are listed in the reference section.

DISCLAIMER

The author has relied heavily upon information supplied orally and in written report form by Dennis LaPrairie, P.Eng., Nevada as well as the geological section of a written report by Robert Cuffney, of Truckee, California who has a Masters Degree in Geological Engineering from Colorado School of Mines. Both these gentlemen have spent a great deal of time on the property doing mapping and sampling and subsequent research.

PROPERTY DESCRIPTION AND LOCATION

The property is located in Sections 28, 27, and 21 in T17N, and R11E, Nevada County, California along the northern border of Placer County, California (Figure 1 and 2). The mine is within the Emigrant Gap Mining District immediately east of Grass Valley and Nevada City Mining Districts and south of Alleghany Mining District (Figure 4). The Bear River, forming the county boundary in this area, flows along the southern portion of the claim group in a southwesterly direction. The Zeibright adits at the south end are located at NTS 4351500N, 696200E; latitude 39º17'26"N, longitude 120º43'34"W. The northern adit, on the Omega property, is located at NTS 4356100N, 693400E; latitude 39º19'52"N, longitude 120º45'18"W.

The lode mining claims are named Steep Hollow #1 through Steep Hollow #7. The county receipts are attached in Appendix 3. The claims were re-staked on February 14, 2003 by Dennis LaPrairie of Reno, Nevada. A total of 7 contiguous claims was staked - each being 457m by 183m (1500 feet long and 600 feet wide) or 83,631 m^2 (900,000 ft^2) or 83.6 hectares (20.66 acres). The California State Bureau of Land Management requires an annual maintenance fee of US$100 unless a Small Miner's Waiver is filed. This can be filed only if the applicant owns fewer than 10 claims nationwide and has performed US$100 worth of assessment work on each claim. This waiver must be accompanied by a US$5.00 fee per claim/site with an Affidavit of Assessment Work (Proof of Labour) Form and, for tunnel sites, a Notice of Intent to Hold. There are currently no land package deals or agreements with any private landholders. Mr. D. LaPrairie, from previous compilation efforts has information on all the landholders in the claim group area for future arrangements.

Figure 2. Claim Location Map

ACCESSIBILITY, CLIMATE, LOCAL RESOURCES, INFRASTRUCTURE AND PHYSIOGRAPHY

The property lies immediately north of the Bear River in the Bear Valley. Interstate 80 runs roughly parallel to the valley in this location south of the river. Highway 20 turns off Interstate 80, the main thoroughfare between Reno, Nevada (100 km, ~60 miles to the east) and Sacramento, California (120 km, ~70 miles to the southwest). A good dirt road runs approximately 4.2 km (2.6 miles) from Interstate 20 into the Donner Mine Camp located at the former Zeibright mining camp. The northern adit, located on the former Omega hydraulic mine property is easily accessed by dirt road leading from Interstate 20 for approximately 3.3 km (2.1 miles).

The regional topography is moderate in the area owing to the location within the foothills of the Sierra Nevada mountain range. The area consists of a series of ridges and valleys. The highest local elevation reaches 6800' asl in Grouse Ridge area approximately 1.6 km (1 mile) north of Lake Spaulding (the dam at Lake Spaulding is at 4600 foot elevation) and 8 km (5 miles) northeast of the Omega property adit. The lowest local elevation is 2600 feet along the South Yuba River at Washington, approximately 5 km (3 miles) northeast of the Omega property adit. The water level elevation along the river continues to decrease as the river flows westward. The topography in the immediate mine area ranges from a minimum of 4120 feet asl at the Omega property northern adit to a maximum of 5200 feet asl approximately halfway between the north and south adits (Figure 2 and 3).

The climate in this area is quite variable due to the variation in topography. At the lower elevations in the region, the temperature rarely rises above 27ºC (80ºF) and rarely dips below -7ºC (20ºF). Summer is dry with occasional showers in June and October. The rest is rainy season and winter. Snow can attain a moderate depth. Abundance of rain and melting snow in the spring give adequate water to the canal systems and artificial reservoirs to supply both irrigation and mining needs (Logan, 1941).

Vegetation supports extensive pine growth with black oak abundant on the ridges and in ravines. At the higher elevations there are extensive forests of white, yellow and sugar pine, spruce and cedar providing timber for the extensive mining operations in the late 1800's and early 1900's (Logan, 1941).

Power and water are easily accessed at the southern end of the property with a main power line running from the Lake Spaulding dams along Interstate 80 and with the Bear River running through the southern portion of the property. If a processing plant were to be built between the Zeibright and Omega adits, power and water would have to be brought in and some sections of road would likely have to be upgraded. In part, for this reason, custom milling is considered a more viable option.

The property's location between Interstate 80 and Interstate 20 allows for a readily accessible human resource from several nearby towns as well as easy access to supplies by road or rail. Should the processing plant be located on the plateau between the two adits, some sections of the road would require upgrading to allow for haulage as well as power to be brought in. Initially, and possibly long term, the ore would be custom milled in either California or Nevada.

HISTORY

The history of the area is fairly extensive. The information is taken from a report written by D. LaPrairie who began assembling property and data on this property in 1988.

Redstone Mine:

Saul Harrison, A.E. Redstone, I.C. Harrison and others staked the first quartz claims in the Zeibright Mine area on April 17, 1858. The location of the Redstone ranch is shown, on surveyed maps, on the present site of the Zeibright Mine.

In April, 1865, there was increased prospecting activity around Gilson's Station, near Interstate 80. By March, 1866, several quartz ledges had been discovered where the outcropping Zeibright Lode passes under Interstate 80 just north of the site of the Redstone Mine.

In July of 1866, mining locations were made by J. Abeel and Dr. S. Palmer, with the Abeel claims covering the Steep Hollow Mine portion of the Zeibright Structure and the Palmer claims covering a parallel vein. There were three Redstones listed as claimants on the Abeel claims and four as claimants on the Palmer claims. J. Abeel was also a claimant on the Palmer claim.

By June of 1867, the Redstones had erected a mill on the Redstone Lode, south of what is now Interstate 80, and J. Teaff (also a claimant on the Palmer claims) had purchased an interest in the properties. By July of 1867, an 8-stamp mill had been operating for several months at the Redstone Mine. Between the Redstone Mine and the Bear River, much prospecting had been undertaken on the extensions of the Redstone. The Blue Bell property underwent working tests of several tons run through the Redstone 2-stamp prospecting mill in Bear Valley. The Steep Hollow Ledge owners (Abeel) were running a tunnel and taking out very rich rock with enough in sight to run a 40-stamp mill.

The United States Minerals Yearbook in 1867 reported that at the Redstone Mine, a depth of 165 feet had been reached and drifts had been run 30 feet on the vein. The rock was very rich and a 4-stamp mill had been running while an 18-stamp mill was being erected. The Redstones had erected a 2-stamp prospecting mill in Bear Valley for prospecting the Champion (later known as the Bonnie Bee) and Blue Bell (known as the Palmer) lodes. By November of 1868, the Champion had an open cut of 65 feet and a tunnel 30 feet farther with rock paying US$45 per ton of free gold. About one fifth of the gross weight of the ore was sulphides that assayed US$225 to the ton. The 65 foot open cut and mill foundations are still in evidence today at the Bonnie Bee Adit on the south side of the Bear River.

A new claim was located by the Blue Bell Company in June, 1871, over the original Harrison (Zeibright) claim and was called the Blue Bell Ledge.

In November, 1874, Mr. Gilson, owner of Gilson's Station since 1866, erected a 40-stamp mill for the Gold Mountain Mining Company north of Redstone Mine.

In 1881, the Redstone's mine in Little Bear Valley had installed an oscillating crusher to pulverize the quartz. From a lot of 7 tons of ore run through the mill in May, US$600 in gold was recovered. In the late 1880's, there was a general depression in the mining industry and it appears that the Redstone mining Company went out of business, allowing all of their claims to lapse.

The Redstone Mine in Blue Canyon was relocated in January, 1885 by Walters and Murphy while P. Boyle relocated the Steep Hollow Creek Mine in January, 1889 on the old tunnel started by O.Gillis on the Abeel claims in 1866. These claims were allowed, once again, to lapse and activity in Bear Valley subsided.

BEAR VALLEY/ZEIBRIGHT MINING COMPANIES:

In January, 1900, Fred Zeitler relocated the original Harrison claims as the "A Quartz Mine" and the witness to posting was W.F. Englebright, both of whom the Zeibright Mine was later named after. Another location by F. Zeitler, named the Robert Quartz Mining Claim, was located in December, 1903, over the original Butts Company location from 1859 and the later Palmer claims from 1866.

Fred Zeitler sold his interests to Fred Searls and W.F. Englebright late in 1903 and evidently disappeared from the Grass Valley area. Zeitler had also been operating the Spanish, Ural, Wyoming, Mayflower and Champion (Nevada City) Mines for the Champion Company at the time of his disappearance. The Zeibright Mining Company formed an operating company named the Bear Valley Mining Company, erected the Zeibright mill and continued developing the property until operations ceased some time prior to 1908 when the Bear Valley Mining Company and property were leased to J. Patrick. The property was leased again in 1914 to W.F. Meeks.

Fred Searls located the Zeibright Extension (Abeel, Boyle) claim in August, 1915, when Meeks turned the Bear Valley Mining Company back to the Zeibright Mining Company. The Bear Valley Mining Company was then leased to F.H. Turner in 1915.

In 1918, the state mineralogist reported that the Bear Valley Mining Company was operating a 30-ton per day mill which consisted of a 10"x 12" jaw crusher, ten 1,150 pound stamps, a classifier with a primary amalgam table and a 4 foot secondary ball mill and amalgam table. An adit (#2 Adit) had been driven 990 feet on the structure and an ore shoot 160 feet long had been stoped to a height of 400 feet. An adit 96 feet lower (#1 Adit) had been advanced to within 100 feet of the ore shoot. The vein was nearly vertical and averaged 20 feet in width. F.H. Turner operated the Zeibright Mine as the Bear Valley Mining Company until about 1923 when he sold it back to the Zeibright Mining Company, still run by Fred Searls. The Zeibright Mining Company lost it's State charter in 1925 and the property lay idle until 1933 when Fred Searls Jr., Vice president of the Empire Star Mines Company (Newmont Mining Corporation) acquired his father's property.

NEWMONT MINING CORPORATION:

Work began in October, 1933 and by February, 1934, Newmont had re-opened the lower (# 1) Adit and had driven a new (# 3) Adit above the old upper (# 2) Adit. The # 1 Adit was 330 feet long in 1933 and had been stoped over approximately half of that length. The upper (#2) Adit was approximately 1,275 feet long at this time. During the 22-month rehabilitation period, the #1 Adit was extended 1,700 feet, a raise driven to the #3 Adit elevation and the #3 Adit was connected to the surface and driven north for a total length of 1,800 feet. A hoisting plant was installed in the #1 Adit and an incline raise was driven to the surface at the #3 Adit for hoisting to the mill.

During the driving of the #1 Adit extension, samples were collected and assayed, long holes were drilled in the rib and chip samples from both levels were taken. Drift rounds on the #1 Adit were hoisted to the mill and processed.

In 1935, Newmont replaced the old mill with a 1,000 ton per day facility composed of two-stage crushing, grinding, jigging and flotation circuits. The jig and flotation concentrates were ground and leached in a 30-ton per day cyanide circuit, which resulted in a recovery rate of 95%. In 1936, 129,886 tons were mined from above the #1 Adit while a 3-compartment shaft was collared in the hanging wall between the #2 and #3 Adits. By the end of 1938, the shaft had been sunk to the 700-foot level and stations were cut on the 300-foot and 550-foot levels. Stoping began on the 300-foot level in mid-1937 and on the 550-foot level late in 1939. Stope progress maps show widths, above the 550-foot level, up to 30 feet with an average of 15 feet. Timbering for ground support was virtually non-existent. By 1939, the total mill throughput was reported to be 800,894 tons of ore with a diluted head grade of about 0.10 ounces gold per ton due to development muck being run through the mill with the ore.

Early in 1940, the tailing impoundment failed and the resultant wash out took out the Pacific Gas and Electric's Drum Power Plant down stream on the Bear River. An injunction was brought against the company curtailing all milling in the valley. Newmont continued to operate the mine for the next two years as a development project only, driving over 25,000 feet of drifts in the mine and sinking the shaft to a depth of 1,930 feet, cutting stations at the 850-foot, 1150-foot, 1450-foot and 1750-foot levels and drifting out on the 850-foot and 1150-foot levels.

The #1 Adit was extended to the north with the intent of connecting up with the Adit being driven south from the Omega Hydraulic pit some 17,000 feet away. The idea was to relocate the mill into the old hydraulic pit to solve the problem of tailings disposal. The #1 Adit was driven 8,500 feet to the north and the Omega Adit was driven 1,800 feet to the south leaving 7,000 feet of haulage tunnel in place. The property was finally shut down completely late in 1941 or early 1942, coinciding with the passage of Executive Order L-208 which cut off all supplies to the gold mined during World War II.

Newmont kept a watchman on the property for several years and re-evaluated it one last time in 1959. They concluded that with US$35 per ounce gold and 0.112 ounces gold per ton head grades, the deposit was too low grade to be mined profitably. Newmont finally disposed of the property in 1959 by deeding all of the mineral rights to the 4,000+-acre property and about 12 acres of surface rights to the Buttes Area Council, Boy Scouts of America. The balance of the surface was sold, without mineral rights, to various different individuals and developers.

LaPrairie Mining began assembling the various mineral and surface rights in mid-1988 and vended the property into Bristlecone Mining Co. Bristlecone Mining Co. was subsequently taken over by Pallas Resource Corp. Pallas Resource Corp. filed for bankruptcy in early 1999, dropping existing leases and mining claims. The claims recently lapsed and were re-staked and the holdings were extended to include potential parallel structures and lateral extensions at both the north and south ends of the known structure. These claims are now held under the name of D. LaPrairie and are to be transferred to Skina Resources Limited.

GEOLOGICAL SETTING

REGIONAL GEOLOGY:

The Sierra Nevada, the dominant mountain range in California, is 640 km (400 miles) long. It has been the dominant source of California's gold production and contains the richest and greatest number of gold mining districts (Bulletin 193, 1970). The main mass of the Sierra Nevada is a huge batholith of granodiorite and related rocks that was intruded into metamorphic rocks of Paleozoic and Mesozoic age. The metamorphic rocks occur largely along the western foothills in the northern end of the range. They are complexly folded and faulted and consist of a number of major metasedimentary and metavolcanic units ranging from the Carboniferous to Upper Jurassic in age (Figure 6 and 8).

In addition, there are numerous intrusions of basic and ultrabasic rocks, many of which are serpentinized. The serpentine bodies appear to have been structurally important in the localization of some gold-bearing deposits and often are parallel to or occur within belts of gold mineralization. Also, there are numerous dioritic and aplitic dikes that are closely associated with gold-bearing veins.

The Zeibright Mine lies within the northern part of the 320 km (200 mile) long Sierra Nevada Foothills Gold Belt, which includes the famous Mother Lode vein system to the south. The regional geologic setting of the northern part of the Foothills Gold Belt is very similar to that of the Mother Lode and many people consider the zone of northern mines to be an extension of the Mother Lode system. The northern zone of mines is a much broader belt than the Mother Lode, reaching 110 km (70 miles) across, near its northern terminus. Gold deposits of the northern mines share many features in common with those of the Mother Lode including similar host rocks, ore and gangue mineralogy, wallrock alteration and tenor of ore. The northern mines, however, differ in general by having more random vein orientations, lesser vein widths, and less common disseminated, or "grey", ore than typical Mother Lode veins.

The Chico Sheet of the Geologic Map of California (1:250,000) (Figure 8 and 9) shows the regional geologic setting of the mine. The Foothills Gold Belt follows the western metamorphic belt along the west flank of the Sierra Nevadas. The Zeibright Mine lies within the central belt of the metamorphic terrane as defined by Schweichert and Cowan (1975). The central belt consists of Paleozoic sediments of the Shoo Fly Complex and a terrane of tectonic melange to the west. The Paleozoic rocks were intensely deformed and metamorphosed during the late Paleozoic, possibly during a compressional event related to the Antler Orogeny. The Melones Fault Zone, a major reverse fault that extends the length of the Foothills Gold Belt, passes less than 4 km (2.5 miles) west of the Zeibright Mine. This fault has been interpreted as a major crustal structure between Paleozoic rocks of the North American Continent on the east and a subducted Jurassic island arc complex on the west, but Schweichert and Cowan (1975) believe that the fault forms the boundary between two related belts of Jurassic rocks. Serpentine (altered peridotite) bodies, localized along the fault zone are believed to represent tectonic slices of the ultra mafic plutonic roots of the island arc. The majority of mines in the Mother Lode occur within or near the Melones Fault Zone or its splays, and the structure appears to have played a major role in the localization of gold deposits.

Quartz monzonite to granodiorite plutons comprising the composite Sierra Nevada batholith intruded the Paleozoic and Mesozoic rocks during the late Jurassic to late Cretaceous time. Granitic rocks outcrop approximately 5 km (3 miles) east of the Zeibright Mine at Lake Spalding and near Emigrant Gap.

Lode Deposits

Much of the gold mineralization is in the belt of metamorphic rocks that extend along the western foothills and in the northern end of the range. The richest as well as the largest number of lode gold deposits are in the northern and central portion of the range. The most productive lode gold districts in the north end of the Sierra Nevada have been the Alleghany, Grass Valley, Johnsville, Nevada City and Sierra City Districts (Figure 4).

Placer Deposits

The alluvial, or placer deposits of the western Sierra Nevada, have contributed more than 40% of California's total gold output. They are divisible into Tertiary (older) deposits, consisting predominantly of quartzitic gravels; and the Quaternary (younger), which are in and adjacent to the present stream channels. The Tertiary channel deposits have been mined by hydraulic and drift mining, while the greatest yield from the Quaternary deposits has been from dredging.

LOCAL GEOLOGY

The Zeibright Mine was the largest producer within the Emigrant Gap mining district, which includes the Red Rock, Texas and Van Avery lode mines, and the Golden Channel, Golden Nugget, Lost Camp, Shell and Wild Yankee placer mines (Clark, 1970). The district lies just southeast of the Washington district where Panorama Resources has defined reserves in excess of 300,000 ounces gold (+5 million tons @ 0.065 ounces gold per ton) at the old Spanish Mine (Cuffney and Woodfill, 1990) which may prove to be an extension of the Zeibright structure. The Grass Valley and Nevada City districts, which contained some of the richest and deepest mines in the Foothills Gold Belt, are located west of the Zeibright Mine.

In the mine area, the pre-Tertiary rocks are exposed only on the lower canyon walls; Tertiary and younger rocks cover the ridges between drainages. Auriferous Eocene gravels of the ancestral Yuba River occur as erosional remnants perched on ridges north and west of the Zeibright Mine. The Omega Mine, a large hydraulic mine about 6 km (3.5 miles) north northwest of the Zeibright Mine, exploited one of the remnant paleochannels (LaPrairie, 1999). Patches of Miocene rhyolitic tuffs, probably derived from sources in Nevada, are preserved locally on the ridges. Thick Pliocene andesitic mudflow breccias, probably representing the volcaniclastic aprons of a series of strato-

volcanoes located somewhat east of the Sierra crest, cover most of the ridges. Pleistocene gravels, deposited as till and outwash from glaciers originating on the Sierra crest also cover portions of the ridges (LaPrairie, 1999).

The Emigrant District is chiefly underlain by thick beds of slate, schist and phyllite of the Carboniferous Blue Canyon Formation. To the north and west, these rocks are overlain by andesite and rhyolite tuff. There are several patches of auriferous Tertiary channel gravels (Figure 8 and 9). There are a number of north-trending quartz veins in schist and slate that contain free gold, pyrite and small amounts of other sulphides. The veins range from 0.3 m to 3.0 m (1 - 10 feet) in thickness and consist of a series of parallel quartz stringers. The milling grade ore usually contained 0.5 ounces per ton gold or less, but some of the ore shoots were extensive (Clark, 1970).

MINE GEOLOGY AND MINERALIZATION:

The Zeibright Mine exploits a NNW-trending veined dike cutting phyllite and schist of the Shoo Fly Complex. The vein is not a simple quartz vein. Rather, it consists of an altered and mineralized dike or sill of granodioritic (?) composition. Texture of the dike ranges from porphyritic-aphanitic to fine-grained equigranular (LaPrairie, 1999). The intrusive body is sill-like, invading weakly discordantly along foliation and bedding of the isoclinally-folded metasediments, which strike N15W to N30W and dip steeply to the west to vertical. The Zeibright dike strikes about N19W where measured in surface stopes. The dike grossly follows the strike of the Shoo Fly metamorphic rocks but on a larger scale is seen to crosscut foliation at a shallow angle and to gradually cut lithologic units on strike.

The dike is highly fractured and strongly veined with milky to clear quartz. Quartz veining observed underground and in surface outcrops ranges from 10% to 40% of the dike. The dike has sharp contacts and the quartz veining is generally restricted to the dike. Minor veining locally penetrates a short distance into the hangingwall, but none has been observed in the footwall (LaPrairie, 1999).

Minor pyrite and arsenopyrite (trace to 0.5%) are disseminated in the quartz veinlets. Greater concentrations of sulphide (several %) are disseminated through the dike, particularly adjacent to the quartz veinlets. Chalcopyrite and pyrrhotite are reported to occur in the ore. Native gold has been reported in the dike on surface outcrop. The quartz veinlets and the intervening dike material are nearly equally mineralized. A recent sampling effort was made to determine if the dike itself was mineralized or if the gold values are contained in the quartz veins within the dike. Rock chip samples were taken of both vein and dike material from surface workings. The following table (from LaPrairie, 1999) shows the results:

NUMBER OF SAMPLES	TYPE OF MATERIAL	RANGE OF ASSAYS Oz gold per ton	AVERAGE ASSAY Oz gold per ton
5	Quartz vein	0.025 - 0.316	0.127
7	Dike(no vein)	0.015 - 0.139	0.066
3	Veined dike	0.068 - 1.860	0.691

Table 1. Recent Sampling Results - Grade with Respect to Material

The unveined dike is strongly mineralized, although the quartz veins carry somewhat higher gold values. The highest grades are associated with the mixed vein and dike material suggesting that the gold is associated with vein selvages or very fine veinlets rather than the thicker quartz veins. This conclusion is supported by the visual identification of free gold within a vein selvage and the

Figure 3. Topographic Section Through Zeibright Mine to Omega Adit

Figure 4. Location of California Gold Districts

Figure 5. Map of Major Rock Units and Lode Gold Belts, N. Sierra Nevada (from Clark, 1970)

common concentration of sulphides adjacent to quartz veins (LaPrairie, 1999). Available mill records from 1939 indicate that 61% of the gold was recovered in the jigging circuit suggesting a large portion of the mineralization occurs as free gold.

The mineralized dike has been measured in 7 locations in natural outcrops and surface stopes and found to vary from 12 feet to over 25 feet in width, averaging 18 feet. Stope widths in the upper levels of the mine indicate similar widths (up to 30 feet). The width of the mineralized dike at depth is uncertain as the 10 foot-wide development drifts rarely cut both walls of the dike.

The Zeibright vein is exposed intermittently for 1,200 feet along the lower part of the north side of the Bear River Canyon. To the north, it is covered by Pliocene mudflows and Pleistocene till. Underground workings driven by Newmont have followed the vein for at least 4,000 feet along strike to the north-northwest and an additional 3,000 feet to the south-southeast. The areas stoped comprise from 60% to 70% of the vein strike length in the mined area. Individual ore shoots have strike lengths of 100 feet to 600 feet and are separated by waste blocks of 100 feet to 300 feet in length. The shoots have great depth persistence, continuing beyond the deepest levels of the mine (1,150 feet below the #1 Adit) (Figure 11).

DEPOSIT TYPES

REGIONAL MODEL

The regional model is based on geological characteristics common to deposit types referred to as any of the following: Mother Lode veins, mesothermal gold-quartz veins, shear-hosted lode gold, low-sulphide gold-quartz veins, or lode gold deposits. The following paragraphs describe the defining features. These are taken from Ash and Aldrick (1996).

Gold-bearing quartz veins and veinlets with minor sulphides crosscut a wide variety of hostrock and are localized along regional faults and related splays. The wallrock is typically altered to silica, pyrite and muscovite within a broader carbonate alteration halo. These deposits range along the Pacific coast from California into northern British Columbia in both Phanerozoic and Archean age settings.

The Phanerozoic-type deposits are contained in moderately- to gently-dipping fault/suture zones related to continental margin collisional tectonism. Suture zones are major crustal breaks, which are characterized by dismembered ophiolitic remnants between diverse assemblages of island arcs, subduction complexes and continental-margin clastic wedges (Ash and Alldrick, 1996).

Veins form within fault and joint systems produced by regional compression or terrane collision. Gold is deposited at crustal levels within and near the brittle-ductile transition zone at depths between 6 and 12 km. Deposits may have a vertical extent of up to 2 km, and lack pronounced zoning (Ash and Alldrick, 1996).

Mineralization is post-peak metamorphism (late syncollisional) with gold-quartz veins particularly abundant in the Late Archean and Mesozoic. In the Phanerozoic setting, within the North America Cordillera, gold veins are post-middle Jurassic and appear to form immediately after accretion of oceanic terranes to the continental margin. In the Mother Lode belt the deposits are Middle-Jurassic (~150 Ma) (Ash and Alldrick, 1996).

The deposit is typically in the form of tabular fissure veins in more competent host rock and as veinlets and stringers forming stockworks in less competent host lithologies. These deposits typically occur as a system of en echelon veins on all scales. Low-grade bulk-tonnage styles of mineralization may develop in areas marginal to veins with gold associated with disseminated

Figure 6. Geologic Map of California

Figure 7. Legend for Figure 6.

Figure 8. Regional Geologic Map, from Chico Quadrangle Sheet

Figure 9. Vertical Section Through Map Area, North of Zeibright Mine (refer to Figure 8).

Figure 10. Legend for Figures 8 and 9.

Figure 11. Longitudinal Cross-Section Through Existing Workings at Zeibright Mine.

sulphides. They may also be related to broad areas of fracturing with gold and sulphides associated with quartz veinlet networks.

Veins generally have sharp contacts with wallrock and exhibit a variety of textures, including massive, ribboned or banded and stockworks with anastimosing gashes and dilations. Textures may be modified or destroyed by subsequent deformation (Ash and Alldrick, 1996).

The gold deposits of the Foothills Gold Belt are mesothermal veins similar in many respects to gold deposits in Archean greenstone belts of the Canadian and Australian shields (Dome, Yellowknife, Kalgoorlie). The origin of the gold deposits is a controversial subject. Four basic theories of the ore genesis have been proposed: syngenetic, plutonic, primary metamorphic and shear-zone metamorphic. Discussion of the theories is beyond the scope of this report. Gold mineralization was likely emplaced between late Jurassic and Cretaceous time in agreement with either plutonic or either metamorphic theories of origin (LaPrairie, 1999).

Typical ore mineralogy for this deposit type includes: native gold, pyrite, arsenopyrite, galena, sphalerite, chalcopyrite, pyrrhotite, tellurides, scheelite, bismuth, cosalite, tetrahedrite, stibnite, molybdenite, gersdorffite (NiAsS), bismuthinite (Bi2S2), tetradymite (Bi2Te2S). Typical gangue mineralogy for this deposit type includes: quartz, carbonates (ferroan-dolomite, ankerite, ferroan-magnesite, calcite, siderite), albite, mariposite (fuchsite), sericite, muscovite, chlorite, tourmaline, and graphite (Ash and Alldrick, 1996).

EXPLORATION

The greatest potential for developing additional reserves at Zeibright lies in exploration of the Zeibright vein both along strike and at depth. Additional ore shoots of similar dimensions to those identified are very likely to occur along strike of the vein. Sampling by Newmont along the 8,500-foot long #1 Adit suggests the existence of at least 3 potentially significant ore shoots, which have not yet been exploited (LaPrairie, 1999). Two other undeveloped ore shoots were encountered in the drift south-southeast of the portal. Continuation of the identified ore shoots to great depth is extremely likely. Ore shoots in the nearby Grass Valley district were followed for over 11,000 feet down dip (LaPrairie, 1999).

The Zeibright vein has sharp hangingwall and footwall contacts and there is little indication of disseminated or “grey” ore in the wallrock. The dike appears to be mineralized due to fracturing produced by the competency contrast between the brittle dike and the relatively ductile schist and phyllite. Stockwork ore may occur adjacent to the mineralized dike where it cuts more competent quartzitic units of the Shoo Fly complex either along strike or at depth. Quartzite was seen outcropping a few hundred feet east of the dike just above the PG&E canal. There are verbal reports from people who worked in the #1 Adit during the drive towards Omega that crosscuts from the Adit encountered massive sulphides (LaPrairie, 1999).

The existence of veins parallel to the Zeibright structure offers exploration opportunities. The limited surface outcrop makes exploration for such deposits difficult, but suggests that veins similar to the Zeibright could well exist undetected in the area. The Zeibright structure was seen to bifurcate north of the highest surface workings (adjacent to the PG&E canal), giving credence to this theory. Underground workings followed the Zeibright structure and little or no crosscutting was done in search of parallel structures.

The total extent of the Zeibright structure is unknown. The mineralized dike may continue along strike beyond the Omega adit. It also extends further to the south-southeast under the Bear River,

as the workings at that end are still on the structure. Further exploration along strike and at depth is warranted.

DRILLING

No drilling has been done on the property. Initial work on the property would involve lateral diamond drilling from underground to identify the potential of parallel structures. Exploration drilling to determine depth continuity of the vein and ore shoots would also be indicated.

PERMITTING

This information is taken from a report prepared by D.LaPrairie for vending purposes at the time.

In Bear Valley, where the Main Shaft and Adits are located, the land status is almost exclusively private in which case the primary agency to be dealt with is the Nevada County Planning Commission who approves or denies Conditional Use Permits for any surface disturbance of more than 1,000 cubic yards of material. Discussions at that time indicated that no permits were required for the rehabilitation of the # 1 Adit. A simple notification was all that was required.

For dewatering the Main Shaft, a National Pollutant Discharge Elimination System Mine Drainage Treatment Permit from the Stat Water Resources Control Board would be required. Sampling of mine water and water from the Bear River indicated that discharge of water into the Bear River may be permissible during high water flow. This sampling would likely have to be redone to determine if those results have changed significantly. An alternative suggested by Mr. LaPrairie was to have land application (sprinklers) set up in the nearby Bear Valley meadows.

Permitting for construction of a milling facility in Bear Valley would be extremely difficult due to zoning, specifically, the amount of private land holdings, in the area. Another option is to build in an area directly above the northern termination of the existing #1 Adit on the Steep Hollow claims. This area, because it is within the National Forest and therefore outside the Nevada County Planning Commission area, is under jurisdiction of the Forest Service. Here, zoning issues do not apply to any construction. Prior to any ore processing plant, decline ramp or tailings impoundment being started, a Plan of Operations and Reclamation Plan is required. Environmental data required for this plan would include hydrology, archaeology, noise, air quality, traffic soil, community impacts and wildlife. However, because construction here would mean that the road would require upgrading and both water and hydro would have to be brought into the property, a more feasible suggestion would be to build the milling facility in the Omega Pit. The most likely option, at this point in time, is to find an operating mill and negotiate a custom milling contract. This eliminates construction costs, rehabilitation and any environmental concerns, either real or perceived.

SAMPLING METHOD AND APPROACH

All sampling data used in this report was taken from previous reports and Newmont Mining Corporation maps. At the time of the author's site visit, the adits were inaccessible to proceed underground. The structure was examined where exposed on surface. Much of the structure between adits has since collapsed due to stoping to near surface from below.

SAMPLE PREPARATION, ANALYSES AND SECURITY

All assays used in these analyses are from Newmont Mining Corporation's maps of level plans and maps. D.LaPrairie and R. Cuffney did some minor sampling, where access permitted, to do a preliminary determination of which part of the veined dike carried the gold values (Table 1).

DATA VERIFICATION

Existing data from Newmont Mining Corporation's maps and sections were used to define extent of workings and the geology of the mine. The assay data used here was tabulated by D. LaPrairie in previous reports on the property. The tabulated data was re-evaluated and weighted and re-arranged (see Tables 4 and 5; Appendices I and II). All interpretations are based on these tables, similarities with nearby properties and the local geology. Geological information was taken from private reports and maps as well as reports and maps published by state and federal agencies. Only one sample was taken for hand sample analysis at the #2 Adit entrance. No further sampling was done at this time due to lack of access to the one available adit. The exposed dike was seen in several locations but due to the amount of collapse from mining below to surface, little detailed examination was possible. Exposure is limited to between adits as there are both Pliocene and Pleistocene deposits capping these rocks in this location.

ADJACENT PROPERTIES

There is little to no data concerning immediately adjacent properties other that a brief description of the Emigrant Gap District in general. Included are brief descriptions of some of the surrounding districts with any production data available. The old Spanish Mine has had recent exploration and a summary of the work and finding is also included. The Spanish Mine is located 8.6km (5.4 miles) to the north-northwest of the Omega property and could possibly be either an extension of or a parallel structure to the Zeibright Structure.

SURROUNDING DISTRICTS

Damascus District: Located approximately 16 km (10 miles) SE of Zeibright Mine and 10 km (7 miles) SE of Dutch Flat District in east-central Placer County. The district hosts the following lode gold mines: Pioneer, Humbug Bar area in north, American Eagle, Black Hawk, Central Dover, Floyn, Lynn, Mars, North Star, Pioneer and Rawhide Mines. There are also extensive placer deposits, which extend from Damascus south. Total production from the Damascus District is approximately $12 million from placer mining and $15 million from lode deposits (Clark, 1970).

The bedrock is slate and schist. The gravels are capped by rhyolite and andesite. The quartz veins, which occur in the slates, range from 0.6 to 2.6 m (2 to 8 feet) in width and contain free gold and often abundant sulphides. The ore is usually low to moderate grade, but the ore shoots had stoping lengths of up to several hundred feet (Clark, 1970).

Dutch Flat District: Located in north central Placer County had significant gold production - all from placer deposits (Clark, 1970).

Emigrant Gap District: Located in east central Placer and Nevada Counties near Emigrant Gap and Blue Canyon includes production from both placer and lode gold deposits. Lode mines include the Zeibright Mine (worked on a large scale in 1930's), Red Rock Mine, Texas Mine and Van Avery Mine (Clark, 1970).

The area is underlain primarily by thick beds of phyllite, slates and schists of the Blue Canyon Formation (Carboniferous). To the north and west, these rocks are overlain by andesite and rhyolite tuff (Clark, 1970).

There are a number of north-trending quartz veins in schist and slate that contain free gold, pyrite and small amounts of other sulphides. The veins range from 0.3 to 3 m (1 to 10 feet) in width and consist of a series of parallel stringers. The milling-grade ore usually contains an estimated 0.5 ounces gold per ton or less, but some of the ore shoots were extensive (Clark, 1970).

Washington District : Located in east-central Nevada county, the district includes the following lode mines: Giant King, Mexican Consolidated, Mount Hope, Red Ledge, Red Paint, Saint Patrick, Spanish and Treasure Box. The district is approximately 29 km (18 miles) NE of Nevada City; at the south end of Goodyear's Bar-Alleghany belt. It also includes the placer diggings at Alpha and Omega mines (Clark, 1970).

Lode mining began in 1850's and continued until 1915. More activity in 1930's with the Red Ridge Mine having more recent activity in the 1950's and 1960's (Clark, 1970) and recent exploration at the Spanish Mine in the 1980's.

The district is underlain chiefly by slate, schist and quartzite of the Blue Canyon Formation (Carboniferous). A serpentine body 1.6 to 3.2 km (1 to 2 miles) wide outcrops in the central portion. The Relief quartzite (Carboniferous) and amphibolite lie to the west and granodiorite to the east (Clark, 1970).

The quartz veins contain small but rich ore bodies, similar to those of the Alleghany District to the north, but are not as plentiful.

Spanish Mine: The Spanish Mine is located in T18N, R11E, Nevada County approximately 8.6km (5.4) north-northwest of the Omega adit. Gold was discovered at the Spanish Mine in 1883 and was mined sporadically until the 1950's at four different sites: the Lower Spanish, Upper Spanish, the Spanish and the West Zone. The property lies within rocks of probable mid-Paleozoic age of the Shoo Fly Formation (Cuffney and Woodfill, 1990).

The property is flanked, along the west, by the Melones Fault - a major structure of regional extent. To the south, along the Mother Lode, the Melones Fault, or its affiliated structures, is host to vein-type gold mineralization. Although gold occurs sporadically along the Melones Fault on the west side of the mine, it is not considered to be the major source of gold on the property. At the Spanish Mine zone, where rock exposure is abundant, the rocks affiliated with gold mineralization are tentatively divided into five types. There are two units referred to in Cuffney and Woodfill (1990) of particular interest. One is referred to as "the Mafic unit" and is described as: "a highly variable sequence of chlorite phyllites containing rare to sparse quartz grains (intermediate to mafic tuffaceous sediments) and porphyritic to equigranular biotite-chlorite-feldspar schist (mafic sills and/or flows). This unit forms an important marker in the southern part of the property, but pinches out north of the Barite Pit." The other unit is termed the "Mine Series" and is described as follows: a complex series of highly altered lenticular beds of black pyretic graphitic phyllite, sericite phyllite, quartz-sericite schist, ferruginous chert (siliceous exhalite), cherty pyretic sericite phyllite (exhalite and tuff) and non-foliated to poorly foliated chlorite-plagioclase schist (mafic sills/flows)." The report also indicates a number of thin, highly clay-altered dikes and sills cut the units and are non-foliated. The dikes and sills are thought to be of Jurassic and Cretaceous age. Lode gold mineralization at the Spanish Mine occurs as both vein gold, disseminated gold and as a component of the massive sulphides.

Genetically, the disseminated gold at the Spanish Mine shows evidence of both syngenetic exhalative and epigenetic vein deposits. Cuffney and Woofill (1990) concluded that there was likely an element of both systems. "The bulk of the gold mineralization may well have been emplaced

syngenetically in an exhalative environment. The present nature of the disseminated gold mineralization may be due to a superposition of a younger Mother-Lode-style mineralizing event that remobilized and probably added some gold to the system." A more recent comment from R.Cuffney, is that the "exhalative" model may not be the actual case. He states that "the gold is generally within or adjacent to a mafic to intermediate sill which intrudes the phyllites. Gold grade appears to be a function of % sulphides in the wallrock and amount of cross-cutting sulphidic quartz stringers in the sill."

These descriptions can well be applied to the geology at the Zeibright Mine. **This data has not been visually confirmed by the author and although it seems comparable to the geology at the Zeibright Mine, the information is not necessarily indicative of the mineralization at the Zeibright Mine.**

MINERAL PROCESSING AND METALLURGICAL TESTING

There has not been any mineral processing or metallurgical testing to date. All production was from the very early 1900's and all that is available are the tons processed with the grades.

MINERAL RESOURCES AND MINERAL RESERVE ESTIMATES

The first two tables presented here are taken directly from D. LaPrairie, 1995. The first of these is based on a long section from Newmont Mining Corporation showing the levels, stoped out areas, average stope widths and the areas on each level considered to have remaining mineable reserves of ore (above 0.080 ounces gold per ton). The following strike lengths and ore shoot lengths are taken from that section. This section was not seen by the author.

LEVEL	MINERALIZED LENGTH (feet)	LENGTH IN ORE (feet)
#3 Adit	2,650	1,580
#1 Adit	2,550	1,870
300 Foot	2,600	2,100
550 Foot	5,200	3,400
850 Foot	4,970	3,420
1150 Foot	4,600	3,320

Table 2. Lengths of Mineralized Structure (from: LaPrairie, 1995).

The data for this second table "were calculated based on length, width and grade of mineable groupings of samples on the 1150 Level." "The samples were listed with a NS co-ordinate, elevation, width and assay. Each sample was assigned a strike length and was given a value based on length x width x assay. These values were then grouped into mineable areas. The length of the ore shoot was divided into the length x width summation of all samples in that shoot to arrive at an average width. The summation of length x width x grade of all samples in the ore shoot were then divided by the average width and the strike length to arrive at the average grade. Six ore shoot with grades of greater than 0.150 ounces gold per ton have been identified on the 1150 Level and are listed here" (LaPrairie, 1995).

From (feet)	To (feet)	Length (feet)	Width (feet)	Grade (oz/ton)
1430N	1376N	57.0	10.0	0.190
828N	313N	516.0	9.5	0.175
19N	97N	116.0	10.0	0.152
121S	287S	165.0	8.8	0.154
400S	484S	83.5	8.7	0.159
1470S	1494S	23.5	9.4	0.154
TOTAL		961.0	9.4	0.168

Table 3. 1150 Level Mineable Ore Shoots (from: LaPrairie, 1995).

The two following tables are merely excerpts from the complete data provided in Appendix I and II. They are the ore-grade sections with weighted averages over both 5 and 10 feet (left in empirical system as original work all in feet). "Newmont Mining Corporation's assay data generated in the period from October, 1933 to February, 1935 consists of samples taken during the re-opening and extension of the #1 Adit and driving of the #3 Adit. During the driving of the #1 Adit extension, samples of 370 back holes from the drift rounds were collected and assayed. Where the vein was wider than the drift (10 feet), 270 long holes were drilled in the rib and cuttings were collected and assayed. In addition, 100 chip samples from both levels were taken. 260 of the drift rounds on #1 Adit were also assayed in the mill and these mill heads were recorded on the plan maps. The available data on the maps from the re-opening of the property generated over 1,200 assays. " (LaPrairie, 1999).
"Other assay data available are 300 chip samples taken from the 1150 foot Level some time after 1941. These samples show widths and grades in ounces Au per ton. Apparently all the levels were sampled at this time. However, only the data from 1150 Level has survived" (LaPrairie, 1999).

The "vein" measured over 10 feet in much of the ore-grade sections and was sampled over its entire width. In the tables, the grades were weighted over both widths for comparison. Where weighted over 5 feet, the grade of any sample widths over 5 feet was left as is; where weighted over 10 feet, the grade of any sample widths over 10 feet was left as is. Where the sample length is in italics, it is because only one end of the sample length was recorded. The value used therefore is double half the distance to the previous sample.

Because this data is all that is available, there is no accurate way to estimate mineral reserves accurately. Statistical analyses, however, are included to give an idea of the potential of this deposit.

	Weighted Grade (/5 feet)	Weighted Grade (/10 feet)	Total Length (feet)	Average Width (feet)	Average Grade (oz/ton)	Average Weighted Grade(/5')	Average Weighted Grade(/10')
	0.140	0.140	57.00	10.00	0.184	0.184	0.184
	0.055	0.028	38.50	4.20	0.116	0.092	0.048
	0.060	0.030	522.50	9.39	0.169	0.167	0.160
	0.140	0.140	325.50	9.26	0.152	0.147	0.135
	0.162	0.081	171.50	8.90	0.137	0.138	0.113
	0.120	0.120	27.50	9.88	0.100	0.100	0.099
	0.140	0.112	58.00	5.93	0.131	0.129	0.078
	0.430	0.430	39.50	10.00	0.198	0.198	0.198
	0.260	0.234	26.00	9.25	0.164	0.164	0.151
TOTAL			**1266.0**				
AVERAGE	**0.154**	**0.141**		**8.53**	**0.150**	**0.147**	**0.130**

Table 4. Ore Grade Assays from #1 Adit (abbreviated from Appendix I)

	Weighted Grade (/10 feet)	Weighted Grade (/5 feet)	Total Length (feet)	Average Width (feet)	Average Grade (oz/ton)	Average Weighted Grade(10')	Average Weighted Grade(5')
	0.140	0.140	86.1	6.2	0.216	0.102	0.159
	0.030	0.060	103.6	6.9	0.126	0.066	0.101
	0.153	0.306	60.5	5.2	0.158	0.075	0.132
	0.100	0.160	74.8	14.1	0.160	0.130	0.160
	0.410	0.410	105.9	13.4	0.118	0.113	0.118
	0.143	0.143	20.5	10.0	0.141	0.141	0.141
	0.183	0.183	88.8	16.2	0.131	0.131	0.131
	0.095	0.105	41.0	11.8	0.169	0.167	0.169
	0.099	0.110	92.7	10.8	0.123	0.114	0.123
	0.039	0.078	139.0	11.1	0.329	0.309	0.325
	0.190	0.190	114.3	11.1	0.137	0.129	0.137
TOTAL			**927.05**				
AVERAGE	**0.132**	**0.151**		**10.621**	**0.164**	**0.134**	**0.154**

Table 5. Ore Grade Assays from 1150 Level (abbreviated from Appendix II)

INTERPRETATION AND CONCLUSIONS

From the data in Tables 4 and 5 it can be seen that there is a total length of 1266 feet on Adit #1 level with ore grade material. The ore grade sections average 8.53 feet in width and grade 0.130 ounces/ton over 10 feet and average 0.147 ounces Au per ton over 5 feet. Similarly, on the 1150 foot Level, there is a total of 927 feet with ore-grade material. The average width of the vein in the ore-grade areas is 10.621 feet with a weighted average grade of 0.134 ounces Au per ton over 10 feet and 0.154 ounces Au per ton over 5 feet. Reliable reserves cannot be determined from these results as there is no data available between levels at this point. This does not diminish the fact that there is significant ore-grade material underground and on at least two levels. Plotting and re-sampling is a priority once underground can be accessed. Once established, these shoots can be drilled from underground drill stations to provide intermediate values upon which more reliable reserves calculations can be based.

Looking at the longitudinal section (Figure 11) many of the mined out stopes can be extrapolated to adjacent levels. This shows a definite 45^{o} to 50^{o} southward plunge to the ore shoots. This can be extended to the ore grade sections on 1150 Level and the Adit #1 Level. Once plotted, and extrapolated, the resulting plan would direct any future exploration/confirmation drilling. Currently, the ore shoots have been followed over a vertical extent of approximately 1800 feet. Because there is no assay data available for the lower levels, this value may be considerably higher.

RECOMMENDATIONS

Several factors need to be considered when preparing the various stages of proposed exploration.

1) Target needs to be defined:

2) further define the existing structure, it's length and ore grades;

3) look for parallel structures to define mining width or

4) both.

5) Thickness of Pliocene mudflows and Pleistocene till need to be considered:

a. drill from surface to determine extent of structure and existence of parallel structures or

b. extend the drifts underground and create underground drilling stations to drill from underground.

6) Extent of land holdings:

7) Expand land holdings both along and across the strike of structure before drilling to ensure a complete land package.

8) Create agreements with surface and mineral rights holders.

9) Determine the extent and grade of structure and possible splays or additional parallel veins before expanding land holdings.

In the author's opinion, due to the variable and irregular width of the veined structure, deep drilling would only confirm structure width and not be a reliable indication for ore reserve calculations. Underground drilling would give the same results and be more cost effective by allowing more and

shorter holes to be drilled. This method would also open the drifts up at the same time to allow bulk samples to be taken for ore definition and metallurgical testwork.

Once underground, extensive detailed sampling across the vein system would be required to determine how grade varies across it and whether there are other mineral associations (as at the Spanish Mine). Some of this has been done as seen in Table 1. Further testing needs to confirm those results over a greater strike length. Structural evaluation is recommended, in particular, looking for evidence of multistage vein emplacement, other fracture systems which may impact on mineralization concentration (i.e. flat veins or intersecting fracture systems).

Given that that the Spanish Mine, only 8.6 km (5.4 miles) away, has had more recent exploration work and reasonable results with similar vein structures, it would seem prudent to extend the land holdings north northwestward towards the Spanish Mine. I would also recommend not expanding across strike until some drill results warrant it. Further staking of ground along strike of the Zeibright structure should be completed to the southeast as well. The dike is known to continue to the south across Bear Creek from lower workings, which connect with the old Bonnie Bee adit.

The Spanish Mine, with considerably less Pliocene mudflows and Pleistocene till cover, have used soil sampling fairly successfully to locate gold-bearing structures. This method might be used with follow-up shallow surface diamond drilling in areas with little cover. This does not occur on the current holdings but may occur if the holdings are extended.

Initially, the Omega adit will have to be re-opened and extended southeastward to allow exploration drilling to locate ore shoots and their vertical extent as well as location/existence of parallel structures. Once access from the southern Zeibright entrance is secured, the main adit will have to be refurbished and existing survey stations identified to confirm sampling data to locate existing ore shoots. Lower stopes are said to have been back-filled with developed ore so, once confirmed, that can be removed and milled to help finance other development.

There are three milling possibilities being considered. The company has identified two potential sites for building its own mill: the existing Omega hydraulic pit is conducive to tailings containment; or the flat high plateau between the Steep Hollow Creek and the North Fork Steep Hollow Creek which lies approximately halfway between the Zeibright and Omega adits. If this second alternative proves viable, access via shaft or ramp would be considered. The ideal solution would be to find a custom milling operation within either California or Nevada. This would eliminate any environmental problems with tailings confinement or wading through the various necessary permitting processes. It would also allow processing of developed ore shoots immediately.

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APPENDIX I - Weighted ore grade assays from Level 1150

				WEIGHTED	WEIGHTED	TOTAL	AVERAGE	AVERAGE	AVERAGE	AVERAGE
DISTANCE	WIDTH	GRADE	LENGTH	GRADE	GRADE	LENGTH	WIDTH	GRADE	WEIGHTED	WEIGHTED
(FEET)	(FEET)	OZ/TON	(FEET)	(/5 FEET)	(/10 FEET)	(FEET)	(FEET)	(OZ/TON)	GRADE(/5')	GRADE(/10')
-1430.0	10.0	0.190	*6.00*	0.190	0.190					
-1424.0	10.0	0.150	6.00	0.150	0.150					
-1418.0	10.0	0.450	7.00	0.450	0.450					
-1410.0	10.0	0.350	6.50	0.350	0.350					
-1405.0	10.0	0.160	6.00	0.160	0.160					
-1398.0	10.0	0.120	6.50	0.120	0.120					
-1392.0	10.0	0.050	5.50	0.050	0.050					
-1387.0	10.0	0.050	6.00	0.050	0.050					
-1380.0	10.0	0.140	7.50	0.140	0.140	57.00	10.00	0.184	0.184	0.184
-1372.0	10.0	0.030	7.50							
-1365.0	7.0	0.070	6.00							
-1360.0	4.0	0.050	5.50							
-1354.0	3.0	0.090	18.50							
-1323.0	3.0	0.070	*10.00*							
-1295.0	3.5	0.180	8.00	0.126	0.063					
-1285.0	4.0	0.060	8.50	0.048	0.024					
-1278.0	5.0	0.130	7.50	0.130	0.065					
-1270.0	6.0	0.100	7.50	0.100	0.060					
-1263.0	2.5	0.110	7.00	0.055	0.028	38.50	4.20	0.116	0.092	0.048
-1192.0	4.0	0.030	*6.00*							
-1186.0	4.0	0.020	15.00							
-1162.0	5.0	0.110	15.50							
-1155.0	4.0	0.170	8.00							
-1146.0	3.5	0.260	*9.00*							
-1104.0	2.5	0.100	*12.00*							
-1092.0	4.5	0.080	8.00							
-1088.0	6.5	0.070	8.00							
-1076.0	1.5	0.040	*12.00*							
-837.0	6.0	0.060	*5.00*							
-832.0	9.0	0.070	6.00							
-825.0	8.5	0.170	6.50	0.170	0.145					
-819.0	9.5	0.280	6.50	0.280	0.266					
-812.0	8.5	0.120	7.00	0.120	0.102					
-805.0	10.0	0.160	6.00	0.160	0.160					
-800.0	10.0	0.400	7.50	0.400	0.400					
-790.0	10.0	0.185	8.50	0.185	0.185					
-783.0	8.0	0.200	7.50	0.200	0.160					
-775.0	8.5	0.100	6.50	0.100	0.085					
-770.0	10.0	0.080	5.50	0.080	0.080					
-764.0	9.0	0.080	6.00	0.080	0.072					
-758.0	8.5	0.340	6.50	0.340	0.289					
-751.0	8.0	0.220	7.00	0.220	0.176					
-744.0	8.0	0.200	6.50	0.200	0.160					
-738.0	9.5	0.160	6.00	0.160	0.152					
-732.0	10.0	0.200	6.00	0.200	0.200					
-726.0	10.0	0.400	11.00	0.400	0.400					
-710.0	10.0	0.280	15.50	0.280	0.280					
				WEIGHTED	WEIGHTED	TOTAL	AVERAGE	AVERAGE	AVERAGE	AVERAGE
DISTANCE	WIDTH	GRADE	LENGTH	GRADE	GRADE	LENGTH	WIDTH	GRADE	WEIGHTED	WEIGHTED

(FEET)	(FEET)	OZ/TON	(FEET)	(/5 FEET)	(/10 FEET)	(FEET)	(FEET)	(OZ/TON)	GRADE(/5')	GRADE(/10')
-688.0	10.0	0.180	6.50	0.180	0.180					
-682.0	10.0	0.020	7.00	0.020	0.020					
-674.0	10.0	0.200	7.50	0.200	0.200					
-667.0	10.0	0.080	7.00	0.080	0.080					
-660.0	10.0	0.120	6.50	0.120	0.120					
-654.0	10.0	0.330	6.50	0.330	0.330					
-647.0	10.0	0.160	7.00	0.160	0.160					
-640.0	10.0	0.180	6.00	0.180	0.180					
-635.0	10.0	0.240	6.00	0.240	0.240					
-628.0	10.0	0.280	7.00	0.280	0.280					
-621.0	10.0	0.320	6.50	0.320	0.320					
-615.0	10.0	0.230	6.00	0.230	0.230					
-609.0	10.0	0.110	6.50	0.110	0.110					
-602.0	9.0	0.080	7.00	0.080	0.072					
-595.0	10.0	0.070	6.00	0.070	0.070					
-590.0	9.0	0.110	4.50	0.110	0.099					
-586.0	10.0	0.100	5.50	0.100	0.100					
-579.0	10.0	0.070	7.00	0.070	0.070					
-572.0	10.0	0.410	6.50	0.410	0.410					
-566.0	9.5	0.420	6.00	0.420	0.399					
-560.0	5.0	0.075	6.50	0.075	0.038					
-553.0	5.0	0.100	6.50	0.100	0.050					
-547.0	8.5	0.190	6.50	0.190	0.162					
-540.0	9.0	0.080	6.50	0.080	0.072					
-534.0	10.0	0.090	6.00	0.090	0.090					
-528.0	10.0	0.210	7.00	0.210	0.210					
-520.0	10.0	0.055	7.50	0.055	0.055					
-513.0	10.0	0.170	7.00	0.170	0.170					
-506.0	10.0	0.100	6.50	0.100	0.100					
-500.0	10.0	0.040	6.50	0.040	0.040					
-493.0	10.0	0.120	7.00	0.120	0.120					
-486.0	10.0	0.060	7.00	0.060	0.060					
-479.0	10.0	0.080	7.50	0.080	0.080					
-471.0	10.0	0.290	7.00	0.290	0.290					
-465.0	10.0	0.220	5.50	0.220	0.220					
-460.0	10.0	0.120	6.50	0.120	0.120					
-452.0	10.0	0.250	7.50	0.250	0.250					
-445.0	10.0	0.100	7.00	0.100	0.100					
-438.0	10.0	0.170	7.00	0.170	0.170					
-431.0	10.0	0.170	7.00	0.170	0.170					
-424.0	10.0	0.110	7.50	0.110	0.110					
-416.0	10.0	0.090	7.00	0.090	0.090					
-410.0	10.0	0.120	7.00	0.120	0.120					
-402.0	10.0	0.190	7.50	0.190	0.190					
-395.0	10.0	0.190	6.00	0.190	0.190					
-390.0	10.0	0.280	5.00	0.280	0.280					
-385.0	10.0	0.170	7.00	0.170	0.170					
-376.0	8.0	0.060	7.50	0.060	0.048					
-370.0	10.0	0.070	6.00	0.070	0.070					
-364.0	10.0	0.090	6.50	0.090	0.090					
-357.0	10.0	0.120	7.00	0.120	0.120					
-350.0	10.0	0.140	7.00	0.140	0.140					
-343.0	10.0	0.090	7.50	0.090	0.090					
-335.0	10.0	0.220	13.50	0.220	0.220					
-316.0	4.0	0.260	12.50	0.208	0.104					
-310.0	2.0	0.150	7.00	0.060	0.030	522.50	9.39	0.169	0.167	0.160
-302.0	2.5	0.120								
				WEIGHTED	WEIGHTED	TOTAL	AVERAGE	AVERAGE	AVERAGE	AVERAGE
DISTANCE	WIDTH	GRADE	LENGTH	GRADE	GRADE	LENGTH	WIDTH	GRADE	WEIGHTED	WEIGHTED
(FEET)	(FEET)	OZ/TON	(FEET)	(/5 FEET)	(/10 FEET)	(FEET)	(FEET)	(OZ/TON)	GRADE(/5')	GRADE(/10')
-230.0	2.5	0.070	*10.00*							

-155.0	5.0	0.200	*10.00*							
-139.0	3.0	0.300	*10.00*							
-50.0	3.5	0.001	*8.00*							
-42.0	6.0	0.060	7.00							
-36.0	3.0	0.310	6.50	0.186	0.093					
-29.0	10.0	0.130	7.00	0.130	0.130					
-22.0	10.0	0.140	6.50	0.140	0.140					
-16.0	10.0	0.150	6.50	0.150	0.150					
-9.0	10.0	0.120	6.00	0.120	0.120					
-4.0	10.0	0.170	5.50	0.170	0.170					
2.0	10.0	0.120	5.00	0.120	0.120					
6.0	10.0	0.300	5.00	0.300	0.300					
12.0	10.0	0.090	5.50	0.090	0.090					
17.0	10.0	0.090	5.50	0.090	0.090					
23.0	10.0	0.160	5.50	0.160	0.160					
28.0	10.0	0.080	6.00	0.080	0.080					
35.0	10.0	0.160	7.00	0.160	0.160					
42.0	10.0	0.240	6.50	0.240	0.240					
48.0	10.0	0.040	6.50	0.040	0.040					
55.0	10.0	0.170	7.00	0.170	0.170					
62.0	10.0	0.220	6.50	0.220	0.220					
68.0	10.0	0.125	6.50	0.125	0.125					
75.0	10.0	0.100	7.00	0.100	0.100					
82.0	10.0	0.090	6.00	0.090	0.090					
87.0	10.0	0.320	6.00	0.320	0.320					
94.0	10.0	0.150	6.50	0.150	0.150					
100.0	10.0	0.080	6.00	0.080	0.080					
106.0	10.0	0.030	9.00	0.030	0.030					
118.0	10.0	0.050	9.50	0.050	0.050					
125.0	10.0	0.240	6.50	0.240	0.240					
131.0	9.0	0.060	9.50	0.060	0.054					
144.0	10.0	0.070	10.00	0.070	0.070					
151.0	10.0	0.060	6.00	0.060	0.060					
156.0	10.0	0.060	5.50	0.060	0.060					
162.0	10.0	0.270	6.50	0.270	0.270					
169.0	10.0	0.320	7.00	0.320	0.320					
176.0	7.0	0.330	7.50	0.330	0.231					
184.0	4.0	0.110	7.00	0.088	0.044					
190.0	3.0	0.300	6.00	0.180	0.090					
196.0	5.0	0.170	6.00	0.170	0.085					
202.0	10.0	0.200	10.50	0.200	0.200					
217.0	10.0	0.090	11.00	0.090	0.090					
224.0	10.0	0.100	7.00	0.100	0.100					
231.0	10.0	0.220	6.00	0.220	0.220					
236.0	10.0	0.130	7.00	0.130	0.130					
245.0	10.0	0.060	5.50	0.060	0.060					
247.0	10.0	0.050	3.50	0.050	0.050					
252.0	10.0	0.120	6.00	0.120	0.120					
259.0	6.5	0.240	7.00	0.240	0.156					
266.0	8.0	0.080	6.00	0.080	0.064					
271.0	10.0	0.190	6.50	0.190	0.190					
				WEIGHTED	**WEIGHTED**	**TOTAL**	**AVERAGE**	**AVERAGE**	**AVERAGE**	**AVERAGE**
DISTANCE	**WIDTH**	**GRADE**	**LENGTH**	**GRADE**	**GRADE**	**LENGTH**	**WIDTH**	**GRADE**	**WEIGHTED**	**WEIGHTED**
(FEET)	**(FEET)**	**OZ/TON**	**(FEET)**	**(/5 FEET)**	**(/10 FEET)**	**(FEET)**	**(FEET)**	**(OZ/TON)**	**GRADE(/5')**	**GRADE(/10')**
279.0	8.0	0.220	6.50	0.220	0.176					
284.0	10.0	0.140	5.00	0.140	0.140	325.50	9.26	0.152	0.147	0.135
289.0	10.0	0.050	5.00							
294.0	10.0	0.090	6.50							

302.0	10.0	0.060	6.00							
306.0	10.0	0.040	5.00							
312.0	10.0	0.070	5.50							
317.0	10.0	0.050	5.00							
322.0	10.0	0.100	5.00	0.100	0.100					
327.0	10.0	0.110	5.00	0.110	0.110					
332.0	10.0	0.060	5.00	0.060	0.060					
337.0	10.0	0.070	5.50	0.070	0.070					
343.0	10.0	0.050	6.50	0.050	0.050					
350.0	10.0	0.110	7.00	0.110	0.110					
357.0	8.0	0.100	7.00	0.100	0.080					
364.0	10.0	0.050	13.50	0.050	0.050					
384.0	10.0	0.050	17.00	0.050	0.050					
398.0	10.0	0.100	9.50	0.100	0.100					
403.0	10.0	0.220	6.00	0.220	0.220					
410.0	10.0	0.110	7.50	0.110	0.110					
418.0	10.0	0.080	7.00	0.080	0.080					
424.0	10.0	0.370	7.00	0.370	0.370					
432.0	10.0	0.040	8.00	0.040	0.040					
440.0	10.0	0.120	7.50	0.120	0.120					
447.0	10.0	0.180	6.00	0.180	0.180					
452.0	10.0	0.070	5.50	0.070	0.070					
458.0	6.0	0.020	5.00	0.020	0.012					
462.0	6.0	0.200	4.50	0.200	0.120					
467.0	7.5	0.030	6.00	0.030	0.023					
474.0	7.0	0.070	6.50	0.070	0.049					
480.0	4.5	0.790	7.00	0.711	0.356					
488.0	4.5	0.180	7.00	0.162	0.081	171.50	8.90	0.137	0.133	0.109
494.0	4.5	0.060	6.00							
500.0	4.0	0.050	6.50							
507.0	5.5	0.080	7.00							
514.0	9.0	0.060	7.00							
521.0	7.0	0.050	5.50							
525.0	10.0	0.050	4.50							
530.0	10.0	0.035	5.50							
536.0	10.0	0.040	5.50							
541.0	10.0	0.030	5.50							
547.0	10.0	0.040	6.00							
553.0	10.0	0.030	6.00							
559.0	10.0	0.040	5.50							
564.0	10.0	0.090	8.50							
576.0	7.5	0.360	10.00							
584.0	9.0	0.020	7.00							
590.0	10.0	0.040	5.00							
594.0	10.0	0.020	5.00							
600.0	8.0	0.100	5.50							
605.0	10.0	0.040	6.00							
612.0	10.0	0.140	7.50							
620.0	10.0	0.030	7.00							
626.0	9.0	0.070	6.00							
632.0	9.0	0.010	5.50							
637.0	10.0	0.030	5.50							
643.0	10.0	0.020	6.50							
				WEIGHTED	**WEIGHTED**	**TOTAL**	**AVERAGE**	**AVERAGE**	**AVERAGE**	**AVERAGE**
DISTANCE	**WIDTH**	**GRADE**	**LENGTH**	**GRADE**	**GRADE**	**LENGTH**	**WIDTH**	**GRADE**	**WEIGHTED**	**WEIGHTED**
(FEET)	**(FEET)**	**OZ/TON**	**(FEET)**	**(/5 FEET)**	**(/10 FEET)**	**(FEET)**	**(FEET)**	**(OZ/TON)**	**GRADE(/5')**	**GRADE(/10')**
650.0	10.0	0.100	6.50							
656.0	10.0	0.050	6.00							
662.0	10.0	0.020	6.50							
669.0	10.0	0.020	6.50							
675.0	10.0	0.030	6.50							
682.0	10.0	0.130	7.00							
689.0	10.0	0.020	7.00							

696.0	10.0	0.020	6.50							
702.0	10.0	0.030	13.00							
722.0	10.0	0.370	14.50							
731.0	10.0	0.005	14.00							
750.0	6.0	0.100	12.50							
756.0	8.0	0.010	7.50							
765.0	9.0	0.100	9.50							
775.0	8.0	0.040	7.50							
780.0	7.0	0.030	5.00							
785.0	4.0	0.060	6.00							
792.0	4.5	0.030	7.50							
800.0	6.0	0.060	7.50							
807.0	8.5	0.090	7.00							
814.0	8.5	0.080	6.50							
820.0	9.5	0.120	6.50	0.120	0.114					
827.0	10.0	0.100	7.50	0.100	0.100					
835.0	10.0	0.060	7.00	0.060	0.060					
841.0	10.0	0.120	6.50	0.120	0.120	27.50	9.88	0.100	0.100	0.099
848.0	9.0	0.160	7.00							
855.0	5.5	0.065	7.00							
862.0	9.0	0.060	5.00							
865.0	10.0	0.050	4.50							
871.0	8.0	0.050	7.00							
879.0	8.0	0.070	7.50							
886.0	8.0	0.100	7.50							
894.0	4.5	0.030	7.00							
900.0	8.0	0.060	5.50							
905.0	8.0	0.030	5.00							
910.0	5.0	0.070	6.00							
917.0	4.5	0.180	7.50	0.162	0.081					
925.0	5.0	0.200	7.50	0.200	0.100					
932.0	6.0	0.060	7.50	0.060	0.036					
940.0	5.0	0.080	11.50	0.080	0.040					
955.0	5.0	0.110	10.00	0.110	0.055					
960.0	8.0	0.150	6.00	0.150	0.120					
967.0	8.0	0.140	8.00	0.140	0.112	58.00	5.93	0.131	0.129	
976.0	8.0	0.030	8.50							
984.0	8.0	0.040	7.00							
990.0	8.0	0.020	6.00							
996.0	6.5	0.040	5.00							
1000.0	8.0	0.015	6.00							
1008.0	10.0	0.060	7.00							
1014.0	10.0	0.190	6.00	0.190	0.190					
1020.0	10.0	0.260	7.50	0.260	0.260					
1029.0	10.0	0.030	7.50	0.030	0.030					
1035.0	10.0	0.080	7.50	0.080	0.080					
1044.0	10.0	0.430	11.00	0.430	0.430	39.50	10.00	0.198	0.198	0.198
1057.0	9.0	0.050	13.00							
1070.0	7.0	0.060	11.00							
1079.0	8.0	0.010	7.50							
				WEIGHTED	**WEIGHTED**	**TOTAL**	**AVERAGE**	**AVERAGE**	**AVERAGE**	**AVERAGE**
DISTANCE	**WIDTH**	**GRADE**	**LENGTH**	**GRADE**	**GRADE**	**LENGTH**	**WIDTH**	**GRADE**	**WEIGHTED**	**WEIGHTED**
(FEET)	**(FEET)**	**OZ/TON**	**(FEET)**	**(/5 FEET)**	**(/10 FEET)**	**(FEET)**	**(FEET)**	**(OZ/TON)**	**GRADE(/5')**	**GRADE(/10')**
1085.0	5.0	0.005	6.00							
1091.0	5.0	0.120	7.50							
1100.0	9.0	0.090	8.00							
1107.0	8.0	0.050	7.50							
1115.0	8.0	0.005	7.50							
1122.0	8.0	0.030	7.50							
1130.0	9.0	0.030	6.00							
1134.0	10.0	0.010	4.50							
1139.0	10.0	0.020	4.00							
1142.0	8.0	0.090	5.00							

1149.0	10.0	0.040	7.00							
1156.0	6.0	0.010	7.50							
1164.0	6.0	0.020	7.00							
1170.0	10.0	0.050	7.50							
1179.0	9.0	0.080	8.00							
1186.0	6.0	0.050	6.50							
1192.0	5.0	0.005	7.00							
1200.0	8.0	0.005	7.50							
1207.0	7.0	0.020	10.50							
1221.0	3.0	0.030	10.00							
1227.0	2.0	0.010	19.00							
1259.0	2.0	0.070	*20.00*							
1369.0	5.0	0.160	*8.00*							
1377.0	5.0	0.110	15.50							
1400.0	2.5	0.030	16.00							
1409.0	3.0	0.060	7.50							
1415.0	2.5	0.060	7.00							
1423.0	5.0	0.020	7.50							
1430.0	5.0	0.020	7.00							
1437.0	9.0	0.040	6.50							
1443.0	8.0	0.060	7.00							
1451.0	8.0	0.030	8.00							
1459.0	9.0	0.090	7.50							
1466.0	9.0	0.080	8.00							
1475.0	10.0	0.150	9.00	0.150	0.150					
1484.0	9.0	0.130	6.00	0.130	0.117					
1487.0	9.0	0.115	5.00	0.115	0.104					
1494.0	9.0	0.260	6.00	0.260	0.234	26.00	9.25	0.164	0.164	0.151
AVERAGE	8.36	0.118		0.154	0.141		8.53	0.150	0.146	0.135
TOTAL	2583.5	36.501	2248.50			1266.00				

APPENDIX II - Weighted ore grade assays from Adit # 1

				WEIGHTED	WEIGHTED	TOTAL	AVERAGE	AVERAGE	AVERAGE	AVERAGE
DISTANCE	**WIDTH**	**GRADE**	**LENGTH**	**GRADE**	**GRADE**	**LENGTH**	**WIDTH**	**GRADE**	**WEIGHTED**	**WEIGHTED**
(FEET)	**(FEET)**	**(OZ/TON)**	**(FEET)**	**(/10 FEET)**	**(/5 FEET)**	**(FEET)**	**(FEET)**	**(OZ/TON)**	**GRADE(10')**	**GRADE(5')**
-1662.0	8.0	0.040								
-1658.0	8.5	0.080	4.0							
-1654.0	8.5	0.070	3.5							
-1651.0	7.0	0.040	2.5							
-1649.0	5.0	0.080	2.5							
-1646.0	3.0	0.130	5.0	0.039	0.078					
-1639.0	1.5	0.100	10.0	0.015	0.030					
-1626.0	1.2	0.320	8.6	0.038	0.077					
-1621.8	0.8	0.132	4.1	0.011	0.021					
-1617.7	0.3	0.070	4.1	0.002	0.004					
-1613.5	3.0	0.225	4.2	0.068	0.135					

-1609.3	3.5	1.260	4.1	0.441	0.882					
-1605.2	5.0	0.456	4.1	0.228	0.456					
-1601.0	6.0	0.040	4.2	0.024	0.040					
-1596.8	7.5	0.285	4.1	0.214	0.285					
-1592.7	7.5	0.040	4.1	0.030	0.040					
-1588.5	8.0	0.110	4.2	0.088	0.110					
-1584.3	7.5	0.041	4.1	0.031	0.041					
-1580.2	8.5	0.090	4.1	0.077	0.090					
-1576.0	8.0	0.220	4.2	0.176	0.220					
-1571.8	13.0	0.100	4.1	0.100	0.100					
-1567.7	14.0	0.120	4.1	0.120	0.120					
-1563.5	14.0	0.140	4.2	0.140	0.140	86.1	6.2	0.216	0.102	0.159
-1559.3	14.0	0.060	4.1							
-1555.2	19.0	0.099	4.1							
-1551.0	18.0	0.040	4.2							
-1546.8	19.0	0.064	4.1							
-1542.7	19.0	0.050	4.1							
-1538.5	21.0	0.080	4.2							
-1534.3	20.0	0.030	4.1							
-1530.2	19.0	0.040	4.1							
-1526.0	20.0	0.010	4.2							
-1521.8	20.0	0.045	4.1							
-1517.7	20.0	0.080	4.1							
-1513.5	20.0	0.070	4.2							
-1509.3	19.0	0.080	4.1							
-1505.2	19.0	0.070	4.1							
-1501.0	18.0	0.150	4.2	0.150	0.150					
-1496.8	15.0	0.050	4.1	0.050	0.050					
-1492.7	13.0	0.090	4.1	0.090	0.090					
-1488.5	9.0	0.060	4.2	0.054	0.060					
-1484.3	9.0	0.030	4.1	0.027	0.030					
-1480.2	8.0	0.100	4.1	0.080	0.100					
-1476.0	8.0	0.130	4.2	0.104	0.130					
-1471.8	5.5	0.080	4.1	0.044	0.080					
-1467.7	5.0	0.320	4.1	0.160	0.320					
-1463.5	4.0	0.140	4.2	0.056	0.112					
-1459.3	3.0	0.070	4.1	0.021	0.042					
-1455.2	2.0	0.100	4.1	0.020	0.040					
-1451.0	4.0	0.220	4.2	0.088	0.176					
-1446.8	7.0	0.090	4.1	0.063	0.090					
-1442.7	7.0	0.160	4.1	0.112	0.160					
-1438.5	7.0	0.100	4.2	0.070	0.100					
-1434.3	7.0	0.060	4.1	0.042	0.060					
-1430.2	7.0	0.050	4.1	0.035	0.050					
-1426.0	5.0	0.060	7.1	0.030	0.060					
				WEIGHTED	**WEIGHTED**	**TOTAL**	**AVERAGE**	**AVERAGE**	**AVERAGE**	**AVERAGE**
DISTANCE	**WIDTH**	**GRADE**	**LENGTH**	**GRADE**	**GRADE**	**LENGTH**	**WIDTH**	**GRADE**	**WEIGHTED**	**WEIGHTED**
(FEET)	**(FEET)**	**(OZ/TON)**	**(FEET)**	**(/10 FEET)**	**(/5 FEET)**	**(FEET)**	**(FEET)**	**(OZ/TON)**	**GRADE(10')**	**GRADE(5')**
-1416.0	3.0	0.100	6.5	0.030	0.060					
-1413.0	2.0	0.500	7.0	0.100	0.200					
-1402.0	2.5	0.120	8.0	0.030	0.060	103.6	6.9	0.126	0.066	0.101
-1397.0	2.5	0.079	4.0							
-1394.0	0.0	0.000	4.4							
-1388.3	0.0	0.000	5.0							
-1384.0	0.0	0.000	4.3							
-1379.7	0.0	0.000	4.4							
-1375.3	0.0	0.000	4.4							
-1371.0	1.5	0.300	4.3	0.045	0.090					
-1366.7	3.0	0.035	4.3	0.011	0.021					
-1362.4	3.0	0.180	4.4	0.054	0.108					
-1358.0	8.0	0.100	4.4	0.080	0.100					
-1353.7	4.0	0.220	4.3	0.088	0.176					
-1349.4	7.0	0.040	4.3	0.028	0.040					
-1345.1	5.5	0.351	4.4	0.193	0.351					

-1340.7	8.0	0.030	4.3	0.024	0.030					
-1336.4	8.0	0.180	4.3	0.144	0.180					
-1332.1	5.5	0.100	4.3	0.055	0.100					
-1327.8	5.5	0.070	4.3	0.039	0.070					
-1323.5	4.0	0.087	4.4	0.035	0.070					
-1319.1	4.0	0.265	4.4	0.106	0.212					
-1314.8	6.0	0.255	4.3	0.153	0.306	60.5	5.2	0.158	0.075	0.132
-1310.5	4.0	0.028	4.3							
-1306.2	4.0	0.040	4.4							
-1301.8	7.0	0.040	4.4							
-1297.5	7.0	0.030	4.3							
-1293.2	7.0	0.140	4.3							
-1288.9	9.0	0.240	4.4							
-1284.5	9.0	0.097	4.4							
-1280.2	12.0	0.030	4.3							
-1275.9	13.0	0.090	4.3							
-1271.6	12.0	0.070	4.3							
-1267.3	12.0	0.030	4.3							
-1262.9	7.0	0.080	4.4							
-1258.6	8.0	0.160	4.3	0.128	0.160					
-1254.3	7.0	0.160	4.3	0.112	0.160					
-1250.0	15.0	0.160	4.4	0.094	0.160					
-1245.6	15.0	0.160	4.4	0.010	0.160					
-1241.3	16.0	0.160	4.3	0.090	0.160					
-1237.0	16.0	0.160	3.1	0.520	0.160					
-1235.0	16.0	0.160	3.0	0.080	0.160					
-1231.1	16.0	0.160	3.9	0.110	0.160					
-1227.2	14.0	0.160	3.9	0.120	0.160					
-1223.2	14.0	0.160	4.0	0.200	0.160					
-1219.3	14.0	0.160	3.9	0.130	0.160					
-1215.4	14.0	0.160	3.9	0.140	0.160					
-1211.5	14.0	0.160	3.9	0.078	0.160					
-1207.6	15.0	0.160	4.0	0.090	0.160					
-1203.6	15.0	0.160	3.9	0.100	0.160					
-1199.7	16.0	0.160	3.9	0.140	0.160					
-1195.8	14.0	0.160	3.9	0.095	0.160					
-1191.9	15.0	0.160	3.9	0.125	0.160					
-1187.9	14.0	0.160	4.0	0.100	0.160	74.8	14.1	0.160	0.130	0.160
-1184.0	14.0	0.070	3.9							
-1180.1	14.0	0.035	3.9							
-1176.2	14.0	0.045	3.9							
-1172.3	14.5	0.060	4.0							
				WEIGHTED	**WEIGHTED**	**TOTAL**	**AVERAGE**	**AVERAGE**	**AVERAGE**	**AVERAGE**
DISTANCE	**WIDTH**	**GRADE**	**LENGTH**	**GRADE**	**GRADE**	**LENGTH**	**WIDTH**	**GRADE**	**WEIGHTED**	**WEIGHTED**
(FEET)	**(FEET)**	**(OZ/TON)**	**(FEET)**	**(/10 FEET)**	**(/5 FEET)**	**(FEET)**	**(FEET)**	**(OZ/TON)**	**GRADE(10')**	**GRADE(5')**
-1168.3	14.0	0.060	3.9							
-1164.4	14.0	0.095	3.9							
-1160.5	13.0	0.087	3.9							
-1156.6	13.0	0.060	3.9							
-1152.7	13.0	0.055	3.9							
-1148.7	13.0	0.040	4.0							
-1144.8	10.0	0.042	3.9							
-1140.9	9.0	0.063	3.9							
-1137.0	9.0	0.025	4.0							
-1133.0	9.0	0.020	4.0							
-1129.1	9.0	0.018	3.9							
-1125.2	9.0	0.070	3.9							
-1121.3	9.0	0.040	3.9							
-1117.4	8.0	0.065	3.9							
-1113.4	8.0	0.050	4.0							
-1109.5	8.0	0.010	3.9							
-1105.6	8.0	0.015	3.9							
-1101.7	8.0	0.010	3.9							
-1097.8	9.0	0.020	4.0							

-1093.8	9.0	0.010	3.9							
-1089.9	10.0	0.012	3.9							
-1086.0	9.0	0.010	3.9							
-1082.1	9.0	0.010	4.0							
-1078.1	9.0	0.010	3.9							
-1074.2	9.0	0.010	3.9							
-1070.3	9.0	0.010	3.9							
-1066.4	9.0	0.010	3.9							
-1062.5	9.0	0.010	4.0							
-1058.5	9.0	0.010	4.0							
-1054.6	9.0	0.010	3.9							
-1050.7	9.0	0.010	3.9							
-1046.8	9.0	0.010	3.9							
-1042.9	9.0	0.036	3.9							
-1038.9	9.0	0.020	4.0							
-1035.0	9.0	0.002	3.9							
-1031.1	9.0	0.002	3.9							
-1027.2	8.0	0.002	3.9							
-1023.3	8.0	0.020	4.0							
-1019.3	8.0	0.041	3.9							
-1015.4	8.0	0.059	3.9							
-1011.5	9.0	0.041	3.9							
-1007.6	9.0	0.015	3.9							
-1003.6	10.0	0.020	3.9							
-999.7	10.0	0.030	3.9							
-995.8	9.0	0.049	3.9							
-991.9	9.0	0.036	3.9							
-988.0	9.0	0.080	3.9							
-984.0	12.0	0.141	3.9	0.141	0.141					
-980.1	16.0	0.154	3.9	0.154	0.154					
-976.2	13.0	0.161	3.9	0.161	0.161					
-972.3	15.0	0.110	3.9	0.110	0.110					
-968.4	17.0	0.069	3.9	0.069	0.069					
-964.4	18.0	0.063	3.9	0.063	0.063					
-960.5	24.0	0.065	3.9	0.065	0.065					
-956.6	24.0	0.117	3.9	0.117	0.117					
-952.7	23.0	0.052	3.9	0.052	0.052					
-948.7	22.0	0.102	4.0	0.102	0.102					
-944.8	19.0	0.064	3.9	0.064	0.064					
				WEIGHTED	**WEIGHTED**	**TOTAL**	**AVERAGE**	**AVERAGE**	**AVERAGE**	**AVERAGE**
DISTANCE	**WIDTH**	**GRADE**	**LENGTH**	**GRADE**	**GRADE**	**LENGTH**	**WIDTH**	**GRADE**	**WEIGHTED**	**WEIGHTED**
(FEET)	**(FEET)**	**(OZ/TON)**	**(FEET)**	**(/10 FEET)**	**(/5 FEET)**	**(FEET)**	**(FEET)**	**(OZ/TON)**	**GRADE(10')**	**GRADE(5')**
-940.9	16.0	0.055	3.9	0.055	0.055					
-937.0	9.0	0.120	3.9	0.108	0.120					
-933.1	9.0	0.064	3.9	0.058	0.064					
-929.1	9.0	0.046	3.9	0.041	0.046					
-925.2	9.0	0.030	3.9	0.027	0.030					
-921.3	9.0	0.125	3.9	0.113	0.125					
-917.4	9.0	0.132	3.9	0.119	0.132					
-913.5	9.0	0.069	3.9	0.062	0.069					
-909.5	9.0	0.105	3.9	0.095	0.105					
-905.6	8.5	0.100	3.9	0.085	0.100					
-901.7	8.5	0.351	3.9	0.298	0.351					
-897.8	10.0	0.120	3.9	0.120	0.120					
-893.9	11.5	0.169	3.9	0.169	0.169					
-889.9	11.5	0.132	3.9	0.132	0.132					
-886.0	10.0	0.069	3.9	0.069	0.069					
-882.1	10.0	0.410	3.9	0.410	0.410	105.9	13.4	0.118	0.113	0.118
-878.2	10.5	0.049	3.9							
-874.2	10.0	0.059	4.0							
-870.3	9.5	0.046	3.9							
-866.4	9.0	0.041	3.9							
-862.5	9.0	0.100	3.9							
-858.6	11.0	0.059	3.9							

-854.6	12.0	0.041	3.9							
-850.7	12.0	0.075	3.9							
-846.8	12.5	0.049	3.9							
-842.9	12.0	0.046	3.9							
-839.0	12.0	0.046	3.9							
-835.0	12.0	0.097	3.9							
-831.1	12.0	0.036	3.9							
-827.2	12.0	0.030	3.9							
-823.3	12.0	0.030	4.0							
-819.3	11.0	1.500	3.9							
-815.4	10.0	0.036	3.9							
-811.5	10.0	0.020	3.9							
-807.6	10.0	0.010	3.9							
-803.7	9.5	0.046	3.9							
-799.7	9.5	0.046	4.0							
-795.8	9.5	0.030	3.9							
-791.9	10.0	0.059	3.9							
-788.0	10.0	0.090	3.9							
-784.1	10.0	0.046	3.9							
-780.1	11.0	0.125	3.9							
-776.2	11.0	0.046	3.9							
-772.3	10.0	0.036	3.9							
-768.4	9.0	0.036	3.9							
-764.4	9.0	0.075	3.9							
-760.5	9.0	0.030	3.9							
-756.6	9.0	0.049	3.9							
-752.7	9.0	0.059	3.9							
-748.8	9.0	0.080	4.0							
-744.8	9.0	0.139	3.9							
-740.9	9.0	0.069	3.9							
-737.0	9.0	0.049	5.9							
-729.0	10.0	0.064	5.7							
-725.6	10.0	0.079	3.4							
-722.2	10.0	0.144	3.4	0.144	0.144					
-718.8	10.0	0.103	3.5	0.103	0.103					
-715.3	10.0	0.124	3.4	0.124	0.124					
				WEIGHTED	**WEIGHTED**	**TOTAL**	**AVERAGE**	**AVERAGE**	**AVERAGE**	**AVERAGE**
DISTANCE	**WIDTH**	**GRADE**	**LENGTH**	**GRADE**	**GRADE**	**LENGTH**	**WIDTH**	**GRADE**	**WEIGHTED**	**WEIGHTED**
(FEET)	**(FEET)**	**(OZ/TON)**	**(FEET)**	**(/10 FEET)**	**(/5 FEET)**	**(FEET)**	**(FEET)**	**(OZ/TON)**	**GRADE(10')**	**GRADE(5')**
-711.9	10.0	0.138	3.4	0.138	0.138					
-708.5	10.0	0.196	3.4	0.196	0.196					
-705.1	10.0	0.143	3.4	0.143	0.143	20.5	10.0	0.141	0.141	0.141
-701.7	11.0	0.062	3.4							
-698.3	12.0	0.065	3.5							
-694.8	13.0	0.053	3.4							
-691.4	13.0	0.056	3.4							
-688.0	14.0	0.058	3.4							
-684.6	15.0	0.100	3.4							
-681.2	16.0	0.085	3.4							
-677.8	17.0	0.084	3.5							
-674.3	17.0	0.087	3.4							
-670.9	17.0	0.087	3.4							
-667.5	17.0	0.066	3.4							
-664.1	17.0	0.060	3.4							
-660.7	17.0	0.233	3.4	0.233	0.233					
-657.3	17.0	0.074	3.4	0.074	0.074					
-653.9	17.0	0.109	3.4	0.109	0.109					
-650.4	16.0	0.075	3.4	0.075	0.075					
-647.0	14.5	0.055	3.4	0.055	0.055					
-643.6	15.0	0.056	3.4	0.056	0.056					
-640.2	17.0	0.090	3.4	0.090	0.090					
-636.8	17.0	0.363	3.4	0.363	0.363					
-633.4	17.0	0.153	3.4	0.153	0.153					
-629.9	17.0	0.100	3.4	0.100	0.100					

-626.5	17.0	0.114	3.4	0.114	0.114					
-623.1	15.5	0.458	3.4	0.458	0.458					
-619.7	17.0	0.076	3.4	0.076	0.076					
-616.3	17.0	0.090	3.4	0.090	0.090					
-612.9	17.0	0.072	3.4	0.072	0.072					
-609.4	17.0	0.047	3.4	0.047	0.047					
-606.0	17.0	0.046	3.4	0.046	0.046					
-602.6	17.0	0.136	3.4	0.136	0.136					
-599.2	17.0	0.186	3.4	0.186	0.186					
-595.8	16.0	0.036	3.4	0.036	0.036					
-592.4	16.0	0.052	3.4	0.052	0.052					
-589.0	16.0	0.076	3.4	0.076	0.076					
-585.5	15.0	0.105	3.4	0.105	0.105					
-582.1	14.0	0.175	3.4	0.175	0.175					
-578.7	14.0	0.247	3.4	0.247	0.247					
-575.3	14.0	0.183	3.4	0.183	0.183	88.8	16.2	0.131	0.131	0.131
-571.9	14.5	0.042	3.4							
-568.5	14.0	0.034	3.4							
-565.0	14.0	0.024	3.4							
-561.6	14.0	0.029	3.4							
-558.2	14.0	0.042	3.4							
-554.8	13.5	0.060	3.4							
-551.4	13.5	0.082	3.4							
-548.0	14.0	0.097	3.4							
-544.6	14.0	0.136	3.4	0.136	0.136					
-541.1	13.5	0.111	3.4	0.111	0.111					
-537.7	13.5	0.081	3.4	0.081	0.081					
-534.3	13.0	0.088	3.4	0.088	0.088					
-530.9	12.0	0.097	3.4	0.097	0.097					
-527.5	12.0	0.172	3.4	0.172	0.172					
-524.1	12.0	0.351	3.4	0.351	0.351					
-520.6	12.0	0.371	3.4	0.371	0.371					
-517.2	11.0	0.171	3.4	0.171	0.171					
				WEIGHTED	**WEIGHTED**	**TOTAL**	**AVERAGE**	**AVERAGE**	**AVERAGE**	**AVERAGE**
DISTANCE	**WIDTH**	**GRADE**	**LENGTH**	**GRADE**	**GRADE**	**LENGTH**	**WIDTH**	**GRADE**	**WEIGHTED**	**WEIGHTED**
(FEET)	**(FEET)**	**(OZ/TON)**	**(FEET)**	**(/10 FEET)**	**(/5 FEET)**	**(FEET)**	**(FEET)**	**(OZ/TON)**	**GRADE(10')**	**GRADE(5')**
-513.8	10.0	0.228	3.4	0.228	0.228					
-510.4	9.0	0.113	3.4	0.102	0.113					
-507.0	9.0	0.105	3.4	0.095	0.105	41.0	11.8	0.169	0.167	0.169
-503.6	10.0	0.073	3.4							
-500.1	10.0	0.066	3.5							
-496.7	13.0	0.051	3.4							
-493.3	13.5	0.080	3.4							
-489.9	14.0	0.082	3.4							
-486.5	13.5	0.022	3.4							
-483.1	14.0	0.028	3.4							
-479.7	15.0	0.044	3.5							
-476.2	14.0	0.049	3.4							
-472.8	13.5	0.036	3.4							
-469.4	13.5	0.029	3.4							
-466.0	14.5	0.138	3.4	0.138	0.138					
-462.6	14.5	0.150	3.4	0.150	0.150					
-459.2	14.5	0.110	3.5	0.110	0.110					
-455.7	14.5	0.144	3.4	0.144	0.144					
-452.3	14.0	0.142	3.4	0.142	0.142					
-448.9	13.0	0.080	3.4	0.080	0.080					
-445.5	12.0	0.056	3.4	0.056	0.056					
-442.1	12.0	0.056	3.4	0.056	0.056					
-438.7	11.0	0.064	3.5	0.064	0.064					
-435.2	10.0	0.237	3.4	0.237	0.237					
-431.8	9.0	0.215	3.4	0.194	0.215					
-428.4	8.0	0.081	3.4	0.065	0.081					
-425.0	8.0	0.100	5.7	0.080	0.100					
-417.0	8.0	0.110	7.5	0.088	0.110					

-410.0	8.0	0.120	8.0	0.096	0.120					
-401.0	8.0	0.161	8.0	0.129	0.161					
-394.0	9.0	0.054	7.0	0.049	0.054					
-387.0	9.0	0.210	8.0	0.189	0.210					
-378.0	9.0	0.110	7.5	0.099	0.110	92.7	10.8	0.123	0.114	0.123
-372.0	9.0	0.059	7.5							
-363.0	9.0	0.064	8.0							
-356.0	9.0	0.080	6.0							
-351.0	9.0	0.049	5.5							
-345.0	9.0	0.030	6.0							
-339.0	10.0	0.015	7.5							
-330.0	12.0	0.020	8.1							
-322.9	12.0	0.028	7.1							
-315.8	13.0	0.042	7.1							
-308.7	13.0	0.035	7.1							
-301.6	11.5	0.046	7.1							
-294.5	12.5	0.070	7.1							
-287.4	13.5	0.443	7.1	0.443	0.443					
-280.3	12.0	0.127	7.1	0.127	0.127					
-273.2	13.0	0.094	7.1	0.094	0.094					
-266.1	13.0	0.182	7.1	0.182	0.182					
-259.0	14.0	0.122	7.1	0.122	0.122					
-252.0	13.5	0.164	7.1	0.164	0.164					
-244.9	12.5	0.102	7.1	0.102	0.102					
-237.8	12.5	0.856	7.1	0.856	0.856					
-230.7	13.8	0.213	7.1	0.213	0.213					
-223.6	11.5	0.103	7.1	0.103	0.103					
-216.5	11.5	0.073	7.1	0.073	0.073					
-209.4	12.5	0.188	7.1	0.188	0.188					
-202.3	11.5	2.388	7.1	2.388	2.388					
				WEIGHTED	**WEIGHTED**	**TOTAL**	**AVERAGE**	**AVERAGE**	**AVERAGE**	**AVERAGE**
DISTANCE	**WIDTH**	**GRADE**	**LENGTH**	**GRADE**	**GRADE**	**LENGTH**	**WIDTH**	**GRADE**	**WEIGHTED**	**WEIGHTED**
(FEET)	**(FEET)**	**(OZ/TON)**	**(FEET)**	**(/10 FEET)**	**(/5 FEET)**	**(FEET)**	**(FEET)**	**(OZ/TON)**	**GRADE(10')**	**GRADE(5')**
-195.2	11.5	0.086	7.1	0.086	0.086					
-188.1	11.5	0.114	7.1	0.114	0.114					
-181.0	10.3	0.108	6.8	0.108	0.108					
-174.5	6.5	0.630	6.8	0.410	0.630					
-167.5	4.0	0.130	9.0	0.052	0.104					
-156.5	3.0	0.130	10.0	0.039	0.078	139.0	11.1	0.329	0.309	0.325
-147.5	2.0	0.049	8.5							
-139.5	1.0	0.049	8.3							
-131.0	1.0	0.059	5.0							
-129.5	1.0	0.049	2.0							
-127.0	2.0	0.059	3.8							
-122.0	2.0	0.080	3.3							
-120.5	2.0	0.090	2.5							
-117.0	2.0	0.080	4.3							
-112.0	3.0	0.260	2.8							
-111.5	3.0	0.049	2.5							
-107.0	4.5	0.269	2.5							
-106.5	6.0	0.046	2.0							
-103.0	7.5	0.230	2.5							
-101.5	8.5	0.041	2.5							
-98.0	9.0	0.069	2.0							
-97.5	9.0	0.030	2.8							
-92.5	9.0	0.041	2.8							
-92.0	9.0	0.030	2.8							
-87.0	9.0	0.059	2.8							
-86.5	9.0	0.090	3.0							
-81.0	9.0	0.041	3.0							
-80.5	9.0	0.100	2.5	0.090	0.100					
-76.0	9.0	0.180	3.0	0.162	0.180					
-74.5	9.0	0.730	2.5	0.657	0.730					
-71.0	9.0	0.090	3.0	0.081	0.090					

-68.5	9.0	0.120	2.5	0.108	0.120					
-66.0	9.0	0.383	3.0	0.345	0.383					
-62.5	9.0	0.049	2.0	0.044	0.049					
-62.0	9.0	0.100	2.3	0.090	0.100					
-58.0	9.0	0.130	2.3	0.117	0.130					
-57.5	9.0	0.169	2.5	0.152	0.169					
-53.0	9.0	0.190	4.8	0.171	0.190					
-48.0	9.0	0.120	2.8	0.108	0.120					
-47.5	9.0	0.049	2.0	0.044	0.049					
-44.0	9.0	0.141	2.0	0.127	0.141					
-43.5	9.0	0.041	2.5	0.037	0.041					
-39.0	10.0	0.200	2.5	0.200	0.200					
-38.5	10.0	0.030	2.5	0.030	0.030					
-34.0	11.0	0.072	5.3	0.072	0.072					
-28.0	12.3	0.134	5.5	0.134	0.134					
-23.0	14.0	0.056	5.0	0.056	0.056					
-18.0	14.5	0.052	4.5	0.052	0.052					
-14.0	14.5	0.034	4.5	0.034	0.034					
-9.0	12.5	0.127	5.0	0.127	0.127					
-4.0	13.5	0.050	5.0	0.050	0.050					
1.0	15.0	0.099	4.5	0.099	0.099					
5.0	14.0	0.115	5.0	0.115	0.115					
11.0	14.5	0.093	5.5	0.093	0.093					
16.0	14.5	0.119	4.5	0.119	0.119					
20.0	13.5	0.144	5.0	0.144	0.144					
26.0	13.0	0.149	5.5	0.149	0.149					
31.0	13.0	0.190	5.0	0.190	0.190	114.3	11.1	0.137	0.129	0.137
				WEIGHTED	**WEIGHTED**	**TOTAL**	**AVERAGE**	**AVERAGE**	**AVERAGE**	**AVERAGE**
DISTANCE	**WIDTH**	**GRADE**	**LENGTH**	**GRADE**	**GRADE**	**LENGTH**	**WIDTH**	**GRADE**	**WEIGHTED**	**WEIGHTED**
(FEET)	**(FEET)**	**(OZ/TON)**	**(FEET)**	**(/10 FEET)**	**(/5 FEET)**	**(FEET)**	**(FEET)**	**(OZ/TON)**	**GRADE(10')**	**GRADE(5')**
TOTAL			1693.5			927.05				
AVERAGE		0.113		0.132	0.151		10.621	0.164	0.134	0.154

Appendix III. California Bureau of Land Management Lode Mining Claim Notices